

# PLASMA DISPLAY PANEL AND DRIVING METHOD THEREOF

## BACKGROUND OF THE INVENTION

### Field of the Invention

This invention relates to a plasma display panel, and  
5 more particularly to a plasma display panel that is capable of improving the discharge efficiency and the brightness. The present invention also is directed to a method for driving the plasma display panel.

### Description of the Related Art

Generally, a plasma display panel (PDP) radiates a fluorescent body by an ultraviolet with a wavelength of 147nm generated during a discharge of He+Xe or Ne+Xe gas to thereby display a picture. Such a PDP is easy to be made into a thin-film and large-dimension type. Moreover, the PDP provides a very improved picture quality owing to a recent technical development. Such a PDP is largely classified into a direct current (DC) type and an alternating current (AC) type. The DC-type PDP causes an opposite discharge between an anode and a cathode provided at a front substrate and a rear substrate, respectively to display a picture. On the other hand, the AC-type PDP allows an AC voltage signal to be applied between electrodes having dielectric layer therebetween to generate a discharge every half-period of the signal, thereby displaying a picture. Such a PDP typically includes an AC-type, surface-discharge PDP that has three electrodes as shown in Fig. 1 and is driven with an AC voltage.

Referring to Fig. 1, a scanning/sustaining electrode 16 and a common sustaining electrode 17 making a sustaining surface-discharge by an application of a AC driving signal are arranged, in parallel, at the rear side of an upper glass substrate 14 constructing the upper substrate 10. The

scanning/sustaining electrode 16 and the common sustaining electrode 17 are transparent electrodes made from indium-tin-oxide (ITO), and metal bus electrodes 20 for supplying AC signals are formed, in parallel, on each of the 5 scanning/sustaining electrode 16 and the common sustaining electrode 17. Because of a high resistance of the transparent electrode, a signal applied from a real external driver is applied, via the metal bus electrode 20, to the transparent electrode of each discharge cell. An upper dielectric layer 18 10 is entirely formed at the rear side of the upper glass substrate 14 provided with the scanning/sustaining electrode 16 and the common sustaining electrode 17. The upper dielectric layer 18 is responsible for accumulating electric charges during the discharge and limiting a discharge current. 15 A protective layer 21 entirely coated on the upper dielectric layer 18 protects the upper dielectric layer 18 from the sputtering during the discharge to prolong a life of the pixel cell as well as to enhance an emission efficiency of secondary electrons, thereby improving a discharge efficiency. On a 20 lower glass substrate 22 constructing the lower substrate 12, an address electrode 22 is arranged perpendicularly to the scanning/sustaining electrode 16 and the common sustaining electrode 17. A lower dielectric layer 26 for forming wall charges during the discharge is entirely coated on the lower glass substrate 22 and the address electrode 24. Barrier ribs 25 26 are vertically formed between the upper substrate 10 and the lower substrate 12. The barrier ribs 32 arranged, in parallel to the address electrode 24, on the lower dielectric layer 26 defines a discharge space 28 along with the upper 30 substrate 10 and the lower substrate 12, and shut off an electrical and optical interference between the adjacent discharge cells. In order to minimize an interference between the adjacent discharge cells, the barrier ribs 32 may be formed in a direction horizontal to the address electrode 24 35 as well as in a direction vertical to the address electrode 24 to have a lattice-shaped structure. A fluorescent material 30 are coated on the surfaces of the lower dielectric layer 26

and the barrier ribs 32. The discharge space 28 is filled with a mixture gas of He+Xe or Ne+Xe.

Referring to Fig. 2, a driving apparatus for the AC-type PDP includes a PDP 40 in which  $m \times n$  discharge cells 44 are arranged in a matrix pattern in such a manner to be connected to scanning/sustaining electrode lines  $Y_1$  to  $Y_m$ , common sustaining electrode lines  $Z_1$  to  $Z_m$  and address electrode lines  $X_1$  to  $X_n$ , a scanning/sustaining electrode driver 36 for driving the scanning/sustaining electrode lines  $Y_1$  to  $Y_m$ , a sustaining electrode driver 34 for driving the common sustaining electrode lines  $Z_1$  to  $Z_m$ , and first and second address electrode drivers 38A and 38B for making a divisional driving of odd-numbered address electrode lines  $X_1, X_3, \dots, X_{n-3}, X_{n-1}$  and even-numbered address electrode lines  $X_2, X_4, \dots, X_{n-2}, X_n$ . The scanning/sustaining electrode driver 36 sequentially applies a scanning pulse and a sustaining pulse to the scanning/sustaining electrode lines  $Y_1$  to  $Y_m$ , thereby allowing the discharge cells to be sequentially scanned line by line and allowing a discharge at each of the  $m \times n$  discharge cells 44 to be sustained. The common sustaining electrode driver 34 applies a sustaining pulse to all of the common sustaining electrode lines  $Z_1$  to  $Z_m$ . The first and second address electrode drivers 38A and 38B supplies an image data to the address electrode lines  $X_1$  to  $X_m$  in such a manner to be synchronized with the scanning pulse. The first address electrode driver 38A supplies the odd-numbered address electrode lines  $X_1, X_3, \dots, X_{n-3}, X_{n-1}$  with an image data while the second address electrode driver 38B supplies the even-numbered address electrode lines  $X_2, X_4, \dots, X_{n-2}, X_n$  with an image data.

Such a PDP driving method typically includes a sub-field driving method in which the address interval and the discharge-sustaining interval are separated. In this sub-field driving method, as shown in Fig. 3, one frame 1F is divided into  $n$  sub-fields SF1 to SF $n$  corresponding to each bit of an  $n$ -bit image data. Each sub-field SF1 to SF $n$  is again divided

into a reset interval RP, an address interval AP and a discharge-sustaining interval SP. The reset interval RP is an interval for initializing a discharge cell, the address interval AP is an interval for generating a selective address discharge in accordance with a logical value of a video data, and the sustaining interval SP is an interval for sustaining a discharge at the discharge cell 44 in which the address discharge has been generated. The reset interval RP and the address interval AP are equally allocated in each sub-field interval. A weighting value with a ratio of  $2^0 : 2^1 : 2^2 : \dots : 2^{n-1}$  is given to the discharge sustaining interval SP to express a gray scale by a combination of the discharge sustaining intervals SP.

Fig. 4 is waveform diagrams of driving signals applied to the PDP during a certain one sub-field interval SF<sub>i</sub>. In the reset interval RP, a priming pulse P<sub>p</sub> is applied to the common sustaining electrode. By this priming pulse P<sub>p</sub>, a reset discharge is generated between each common sustaining electrode Z<sub>m</sub> and each scanning/sustaining electrode Y<sub>1</sub> to Y<sub>m</sub> of the entire discharge cells to initialize the discharge cells. At this time, a voltage pulse lower than the priming pulse P<sub>p</sub> is applied to the address electrode A<sub>n</sub> so as to prevent a discharge between the address electrode A<sub>n</sub> and the common sustaining electrode Z<sub>m</sub>. By the reset discharge, a large amount of wall charges are formed at the common sustaining electrode Z<sub>m</sub> and the scanning/sustaining electrode Y<sub>1</sub> to Y<sub>m</sub> of each discharge cell. Subsequently, a self-erasure discharge is generated at the discharge cells by the large amount of wall charges to eliminate the wall charges and leave a small amount of charged particles. These small amount of charged particles help an address discharge in the following address interval. In the address interval AP, a scanning voltage pulse -V<sub>s</sub> is applied line-sequentially to the first to m<sup>th</sup> scanning/sustaining electrodes Y<sub>1</sub> to Y<sub>m</sub>. At the same time, a data pulse V<sub>d</sub> according to a logical value of a data is applied to the address electrodes A<sub>n</sub>. Thus, an address discharge is generated at discharge cells to which the

scanning voltage pulse  $-V_s$  and the data pulse  $V_d$  are simultaneously applied. Wall charges are formed at the discharge cells in which the address discharge has been generated. During this address interval AP, a desired constant voltage is applied to the common sustaining electrodes  $Z_m$  to prevent a discharge between each address electrode  $A_n$  and each common sustaining electrode  $Z_m$ . In the sustaining interval SP, a sustaining pulse  $S_p$  is alternately applied to the first to  $m^{\text{th}}$  scanning/sustaining electrodes  $Y_1$  to  $Y_m$  and the common sustaining electrodes  $Z_m$ . Accordingly, a sustaining discharge is generated continuously only at the discharge cells formed with the wall charges by the address discharge to emit a visible light.

The AC-type PDP driven in this manner still requires to overcome several factors causing deterioration in the efficiency and the brightness. In the AC-type PDP as shown in Fig. 1, the scanning/sustaining electrode  $Y_m$  and the common sustaining electrode  $Z_m$  causing a sustaining surface-discharge are arranged in such a manner to be spaced at a short distance within a narrow discharge cell. When a scanning voltage pulse is alternately applied to the scanning/sustaining electrode  $Y_m$  and the common sustaining electrode  $Z_m$ , a discharge is initiated at a gap between the two electrodes and then a discharge area is enlarged into the surfaces of the two electrodes.

However, in such an AC-type PDP structure, since a distance between the scanning/sustaining electrode  $Y_m$  and the common sustaining electrode  $Z_m$  is short, a discharge path upon sustaining discharge is short to generate a small quantity of ultraviolet rays and a light-emission area within the discharge cell is extremely limited. This causes a deterioration of brightness.

Also, the AC-type PDP structure has a problem in that, as a distance between the scanning/sustaining electrode  $Y_m$  and the common sustaining electrode  $Z_m$  is increased so as to

increase the discharge path and the light-emission area, an erroneous discharge with other adjacent cells is generated. Furthermore, a ratio of time contributing to a real light-emission in the entire sustaining interval during the sustaining period determining the brightness of the PDP is very low to cause a deterioration in the efficiency and the brightness.

A pulse width of the sustaining pulse alternately applied to the scanning/sustaining electrode  $Y_m$  and the common sustaining electrode  $Z_m$  in the sustaining interval  $SP$  is several  $\mu s$ . But, since a discharge is really generated only at a short instant supplied with a pulse, a time contributing to a real light-emission becomes merely  $1\mu s$  for each pulse. The discharge is generated once only at a very short instant for a single pulse while charged particles produced upon discharge in the remaining time are moved along the discharge path in accordance with the polarity of the electrode to form wall charges at the surface of the dielectric layer positioned at the lower portion of the electrode. Thus, an electric field at the discharge space is lowered and a discharge voltage is decreased, to thereby stop the discharge. As a result, since the major time of the sustaining interval  $SP$  is wasted for a formation of wall charges and a preparation for the next discharge, the entire sustaining interval fails to be exploited efficiently, thereby causing a deterioration in the discharge and light-emission efficiency and the brightness.

#### **SUMMARY OF THE INVENTION**

Accordingly, it is an object of the present invention to provide a plasma display panel (PDP) wherein a discharge distance is increased to make a high efficiency, a light-emission area is enlarged to obtain a high brightness, and a light-emission time is increased to improve a light-emission efficiency.

A further object of the present invention is to provide a PDP driving method wherein said PDP can be driven by an active system.

In order to achieve these and other objects of the invention, a plasma display panel according to one aspect of the present invention includes sustaining electrodes formed at the boundary portions between the discharge cells; and trigger electrodes formed at the inner sides of the discharge cells.

A method of driving a plasma display panel according to another aspect of the present invention includes the steps of applying a reset pulse to sustaining electrodes during a reset period; applying a scanning pulse to trigger electrodes during an address period; applying a first sustaining pulse to the trigger electrodes during a sustaining period; and applying a second sustaining pulse to the sustaining electrodes in such a manner to be alternate with the first sustaining pulse.

A method of driving a plasma display panel according to still another aspect of the present invention includes a first sub-field for applying a scanning voltage pulse to odd-numbered trigger electrodes during an address period; and a second sub-field for applying a scanning voltage pulse to even-numbered trigger electrodes during the address period.

A method of driving a plasma display panel according to still another aspect of the present invention includes a first sub-field for applying a scanning voltage pulse to even-numbered trigger electrodes during an address period; and a second sub-field for applying a scanning voltage pulse to odd-numbered trigger electrodes during the address period.

#### **BRIEF DESCRIPTION OF THE DRAWINGS**

These and other objects of the invention will be apparent from the following detailed description of the embodiments of the present invention with reference to the accompanying drawings, in which:

Fig. 1 is a vertical section view showing a structure of a discharge cell of a conventional AC surface-discharge plasma display panel;

5 Fig. 2 is a plan view representing an arrangement of the pixel cells and the electrode lines of the AC-type plasma display panel shown in Fig. 1;

Fig. 3 illustrates a configuration of one frame for providing a gray level display of the plasma display panel shown in Fig. 1;

10 Fig. 4 is waveform diagrams of driving signals applied to the plasma display panel during a certain sub-field interval shown in Fig. 3;

15 Fig. 5 is a vertical section view showing a discharge cell structure of an AC surface-discharge plasma display panel according to a first embodiment of the present invention;

Fig. 6 is a plan view representing an arrangement of the pixel cells and the electrode lines of the AC-type plasma display panel shown in Fig. 5;

20 Fig. 7 is waveform diagrams of driving signals applied to the AC-type plasma display panel shown in Fig. 5;

Fig. 8 is a section view showing a discharge cell structure of an AC surface-discharge plasma display panel according to a second embodiment of the present invention;

25 Fig. 9 is a plan view showing a structure of an AC surface-discharge plasma display panel according to a third embodiment of the present invention;

Fig. 10 and Fig. 11 are waveform diagrams of an example of driving signals applied to the AC surface-discharge plasma display panel shown in Fig. 9; and

30 Fig. 12 and Fig. 13 are waveform diagrams of another example of driving signals applied to the AC surface-discharge plasma display panel shown in Fig. 9.

#### **DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT**

35 Fig. 5 is a vertical section view showing a discharge cell structure of an AC surface-discharge plasma display panel (PDP) according to a first embodiment of the present

invention. Referring to Fig. 5, the AC surface-discharge PDP includes a nth sustaining electrode Sn provided at the rear side of an upper glass substrate 74 at a boundary portion between a (n-1)th discharge cell Cn-1 and a nth discharge cell 5 Cn, and a nth trigger electrode Tn provided at the rear side of the upper glass substrate 74 in such a manner to be spaced at a small distance from the nth sustaining electrode Sn at the nth discharge cell Cn in order to cause a primary sustaining discharge along with the nth sustaining electrode 10 Sn.

As shown in Fig. 5, the nth trigger electrode Tn is arranged between the nth sustaining electrode Sn and a (n+1)th sustaining electrode Sn+1, and a distance between the nth trigger electrode Tn and the (n+1)th sustaining electrode Sn+1 is set to be larger than that between the nth sustaining electrode Sn and the nth trigger electrode Tn. The trigger electrodes Tn and Tn+1 and the sustaining electrodes Sn and Sn+1 are transparent electrodes made from indium-tin-oxide (ITO) so as to prevent a deterioration in the brightness of 15 the PDP. 20

In the conventional three-electrode structure, a sustaining electrode pair of the scanning/sustaining electrode Ym and the common sustaining electrode Zm are provided at the upper substrate of the discharge cell to cause a sustaining 25 discharge between the two electrodes Ym and Zm. On the other hand, in the present invention, three electrodes of the nth sustaining electrode Sn serving as the first sustaining electrode, the (n+1)th sustaining electrode Sn+1 serving as the second sustaining electrode and the nth trigger electrode 30 Tn cause a sustaining electrode at the nth discharge cell Cn. Meanwhile, since the sustaining electrodes Sn and Sn+1 are formed at the boundary portion between the adjacent discharge cells, two discharge cells Cn-1 and Cn or Cn and Cn+1 have such a structure that they share the sustaining electrode Sn 35 or Sn+1, respectively. In other words, the (n-1)th discharge cell Cn-1 shares the nth sustaining electrode Sn with the nth

discharge cell  $C_n$ , and the  $n$ th discharge cell  $C_n$  shares the  $(n+1)$ th sustaining electrode  $S_{n+1}$  with the  $(n+1)$ th discharge cell  $C_{n+1}$ . The  $n$ th sustaining electrode  $S_n$  serves as the first sustaining electrode causing a primary sustaining discharge 5 along with the  $n$ th trigger electrode  $T_n$  at the  $n$ th discharge cell  $C_n$  while serving as the second sustaining electrode causing a secondary sustaining discharge along with the  $(n-1)$ th trigger electrode  $T_{n-1}$  at the  $(n-1)$ th discharge cell  $C_{n-1}$ . Likewise, the  $(n+1)$ th sustaining electrode  $S_{n+1}$  serves as 10 the second sustaining electrode causing a second sustaining discharge along with the  $n$ th trigger electrode  $T_n$  after the primary sustaining discharge at the  $n$ th discharge cell  $C_n$  while serving as the first sustaining electrode causing a first sustaining discharge at the  $(n+1)$ th discharge cell  $C_{n+1}$ . At the rear side of the upper glass substrate provided with 15 these electrodes, the upper dielectric layer 78 is formed to have a desired thickness.

Other structures and features except for the structure of the sustaining electrodes provided at the upper substrate 70 are identical to those of the conventional three-electrode, AC 20 surface-discharge PDP. More specifically, a MgO protective layer 80 for protecting the upper substrate 70 from a discharge sputtering is formed at the rear side of the upper dielectric layer 78. An address electrode 86 is formed in a 25 direction perpendicular to the sustaining electrode  $S_n$  and the trigger electrode  $T_n$  provided at the upper substrate 70 on a lower glass substrate 82 constituting a lower substrate 72. A lower dielectric layer 84 is formed on the lower glass substrate 82 provided with the address electrode 86. As shown 30 in Fig. 6, barrier ribs 92 are formed on the lower substrate 72 provided with the lower dielectric layer 84 in directions parallel to and perpendicular to the address electrode 86.

In the first embodiment, as shown in Fig. 6, the barrier ribs 92 are formed in a lattice shape so as to minimize 35 electrical and optical interference between the adjacent cells positioned at the up, down, left and right sides upon their

formation. In this case, the barrier rib 92 is formed at each boundary portion of the scanning lines to position the nth sustaining electrode Sn and the (n+1)th sustaining electrode Sn+1 on the barrier ribs 92. A discharge space 88 surrounded by the upper substrate 70, the lower substrate 72 and the barrier ribs 92 is filled with a mixture gas of He+Xe or Ne+Xe. In Fig. 6, a discharge cell 94 is positioned at each intersection among the sustaining electrode S1 to Sn, the trigger electrodes T1 to Tn and the address electrodes A1 to An.

Fig. 7 shows a method of driving an AC surface-discharge PDP according to a first embodiment of the present invention.

Referring now to Fig. 7, one sub-field is divided into a reset interval RP for initializing all of the discharge cells, an address interval AP for selecting a discharge cell to be turned on and a sustaining interval SP for sustaining a discharge at the discharge cell selected in the address interval AP. First, in the reset interval RP, a reset pulse is applied to each sustaining electrode line Sn and SDn+1 to generate a reset discharge. In the address interval AP, a scanning voltage pulse -Vs is sequentially applied to the trigger electrode Tn for each sustaining electrode line Sn and Sn+1 and a data pulse Vd is applied to the address electrode An in synchronization with the scanning voltage pulse, thereby generating an address discharge at the discharge cells supplied with a data. The discharge cell selected by the address discharge sustains a discharge in the following sustaining interval SP to emit a light. In the sustaining interval SP, a sustaining pulse Vsus is alternately applied to the trigger electrode Tn and the sustaining electrodes Sn and Sn+1. At this time, a sustaining discharge is generated only at the discharge cells selected by a voltage difference Vsus between the trigger electrode Tn and the sustaining electrodes Sn and Sn+1. As shown in Fig. 7, the same sustaining waveform is applied to the nth sustaining electrode Sn and the (n+1)th sustaining electrode Sn+1 at the nth discharge cell Cn. During

the sustaining interval  $SP$ , twice sustaining discharge is generated between three electrodes of the  $n$ th sustaining electrode  $Sn$ , the  $n$ th trigger electrode  $Tn$  and the  $(n+1)$ th sustaining electrode  $Sn+1$ . More specifically, a primary sustaining discharge is generated between the  $n$ th discharge-sustaining electrode  $Sn$  and the  $n$ th trigger electrode  $Tn$  having a narrow distance from each other by a voltage difference  $V_{sus}$ . This primary sustaining discharge forms wall charges and charged particles at the discharge space 88. Next, a voltage derived from the wall charges and the charged particles formed by the primary sustaining discharge is added to the sustaining voltage  $V_{sus}$  between the  $n$ th trigger electrode  $Tn$  and the  $(n+1)$ th sustaining electrode  $Sn+1$  to form a higher discharge voltage within the discharge cell, thereby generating a secondary sustaining voltage between the  $n$ th trigger electrode  $Tn$  and the  $(n+1)$ th sustaining electrode  $Sn+1$  having a relatively long distance from each other. In other words, a primary discharge between the  $n$ th sustaining electrode  $Sn$  and the  $n$ th trigger electrode  $Tn$  serves as a priming discharge of the secondary discharge generated between the  $n$ th trigger electrode  $Tn$  and the  $(n+1)$ th sustaining electrode  $Sn+1$  having a long distance from each other.

In the present invention, twice discharge is generated for each sustaining pulse by such a driving method. This obtains an effect of increasing a discharge frequency in the sustaining interval into two times in comparison to the conventional three-electrode PDP in which once discharge is generated for each sustaining pulse. Accordingly, in the present PDP, a discharge efficiency can be not only largely increased, but also the brightness of the PDP caused by the sustaining discharge can be largely improved when compared with the conventional three-electrode structure. Furthermore, since a discharge is generated between the  $n$ th trigger electrode  $Tn$  and the  $(n+1)$ th sustaining electrode  $Sn+1$  having a relatively long distance from each other, a discharge path is more lengthened than that in the prior art to increase a generated quantity of an ultraviolet ray and a real light-

emission area is much more enlarged than that in the prior art to permit a realization of a high efficiency and a high brightness.

5 Fig. 8 shows a discharge cell structure of a AC surface-discharge PDP according to a second embodiment of the present invention.

10 The second embodiment has a difference from the first embodiment in that a metal bus electrode 76 having a light-shielding property is formed at each center of the rear sides of sustaining electrodes  $S_n$  and  $S_{n+1}$  and trigger electrodes  $T_n$  and  $T_{n+1}$ . Other elements and features in the second embodiment are identical to those in the first embodiment.

15 A driving method for the second embodiment of the present invention is identical to that for the first embodiment shown in Fig. 1. In the sustaining interval SP after an address discharge, a primary priming discharge is generated between the  $n$ th sustaining electrode  $S_n$  and the  $n$ th trigger electrode  $T_n$  having a narrow distance from each other at the  $n$ th discharge cell  $C_n$ . Subsequently, a secondary sustaining discharge having a long discharge path is generated between the  $(n+1)$ th sustaining electrode  $S_{n+1}$  and the  $n$ th trigger electrode  $T_n$ . The second embodiment of the present invention also generates twice discharge every sustaining pulse to improve the brightness. Furthermore, the second embodiment has 20 a long discharge path and an enlarged light-emission area so that it can realize a high efficiency and a high brightness. In addition, the second embodiment has the light-shielding bus electrode 76 formed at the center of each sustaining electrode  $S_n$  and  $S_{n+1}$ , so that it can prevent a resolution caused by an 25 optical interference from being deteriorated at the boundary portion between the emitted cell and the non-emitted cell. Moreover, it can reduce a deterioration of a black color 30 display quality.

Fig. 9 shows a structure of an AC surface-discharge PDP according to a third embodiment of the present invention.

When the third embodiment shown in Fig. 9 is compared with the first embodiment shown in Fig. 6, it has a structure in which any horizontal barrier ribs does not exist between the scanning lines. As mentioned above, a sustaining discharge at the nth discharge cell  $C_n$  is caused by three electrodes of the nth sustaining electrode  $S_n$ , the nth trigger electrode  $T_n$  and the  $(n+1)$ th sustaining electrode  $S_{n+1}$  to achieve a high efficiency and a high brightness. Since the third embodiment has barrier ribs taking a stripe shape rather than a lattice shape, it has an advantage in that a panel structure and a manufacturing process can be simplified. However, the PDP according to the third embodiment does not have any horizontal barrier ribs for dividing the sustaining electrode lines  $S_1, S_2, S_3, S_4, \dots$ , but has only vertical barrier ribs 92 formed in a direction parallel to the address electrodes  $A_1$  to  $A_n$ . Red (R), green (G) and blue (B) pixels arranged horizontally along the address electrode lines  $A_1$  to  $A_n$  at a single sustaining electrode line are divided by the vertical barrier ribs 92 to prevent an erroneous discharge between the pixels. But, an erroneous discharge may be generated between discharge cells positioned at the adjacent sustaining electrode lines. In order to prevent such an erroneous discharge, a driving method as shown in Fig. 10 to Fig. 13 is utilized.

Fig. 10 and Fig. 11 are waveform diagrams for explaining an example of driving methods applied to the AC surface-discharge PDP according to the third embodiment of the present invention.

Referring to Figs. 10 and 11, the trigger electrode lines are divided into odd-numbered trigger electrode lines  $T_n$  and even-numbered trigger electrode lines  $T_{n+1}$  for a driving. In Fig. 10, a reset pulse  $R_p$  is first applied to each sustaining electrode  $S_n$  and  $S_{n+1}$  upon driving of the odd-numbered trigger electrode lines  $T_n$  to entirely cause a reset discharge. Next,

5 a sustaining pulse  $-Vs$  is applied to the odd-numbered trigger electrode line  $T_n$  and, at the same time, a data pulse is applied to each address electrode  $A_n$ , thereby generating an address discharge at the discharge cell  $C_n$  provided with the odd-numbered trigger electrode line  $T_n$ . A discharge is sustained in the following sustaining interval  $SP$  at the discharge cells  $C_n$  of the odd-numbered trigger electrode lines  $T_n$  selected by the address discharge. During the sustaining interval  $SP$ , a sustaining discharge is generated only at the 10 discharge cells  $C_n$  of the odd-numbered trigger electrode lines  $T_n$ . To this end, a sustaining pulse  $V_{sus}$  is alternately applied to the odd-numbered electrode line  $T_n$  and the sustaining electrode lines  $S_n$  and  $S_{n+1}$ , and a voltage waveform identical to a waveform applied to the sustaining electrodes  $S_n$  and  $S_{n+1}$  is applied to the even-numbered trigger electrode line  $T_{n+1}$ . Accordingly, a primary sustaining discharge is generated at the discharge cells provided with the odd-numbered trigger electrode line  $T_n$  due to voltage differences  $V_{sus}$  between the odd-numbered trigger electrodes  $T_1, T_3, T_5, \dots$  and the first sustaining electrodes  $S_1, S_3, S_5, \dots$  Then, 15 a voltage caused by charged particles produced at this time is added to a voltage difference between the trigger electrodes  $T_1, T_3, T_5, \dots$  and the second sustaining electrodes  $S_2, S_4, S_6, \dots$  to cause a secondary long-distance sustaining 20 discharge. However, since a voltage difference between the even-numbered trigger electrodes  $T_2, T_4, T_6, \dots$  and the sustaining electrodes  $S_1$  to  $S_{n+1}$  is not generated at the discharge cells of the even-numbered trigger electrode  $T_{n+1}$ , a 25 sustaining discharge is not generated.

30 Similarly, a driving waveform as shown in Fig. 11 is applied to each electrode upon driving of the even-numbered trigger electrode line  $T_{n+1}$ . First, a reset pulse  $R_p$  is applied to each sustaining electrode  $S_n$  and  $S_{n+1}$  to entirely cause a reset discharge. Next, a scanning voltage pulse  $-Vs$  is 35 applied to the even-numbered trigger electrode line  $T_{n+1}$  and, at the same time, a data pulse  $V_d$  is applied to each address electrode  $A_n$ , thereby generating an address discharge at the

discharge cells  $C_{n+1}$  provided with the even-numbered trigger electrode line  $T_{n+1}$ . A discharge is sustained in the following sustaining interval  $SP$  at the discharge cells  $C_{n+1}$  provided with the even-numbered trigger electrode lines  $T_{n+1}$  selected by the address discharge. During the sustaining interval  $SP$ , a sustaining discharge is generated only at the discharge cells  $C_{n+1}$  provided with the even-numbered trigger electrode lines  $T_{n+1}$ . To this end, a sustaining pulse  $V_{sus}$  is alternately applied to the even-numbered electrode line  $T_{n+1}$  and the sustaining electrode lines  $S_n$  and  $S_{n+1}$ , and a voltage waveform identical to a waveform applied to the sustaining electrodes  $S_n$  and  $S_{n+1}$  is applied to the odd-numbered trigger electrode line  $T_n$ . Accordingly, a primary sustaining discharge is generated at the discharge cells  $C_{n+1}$  provided with the even-numbered trigger electrode line  $T_{n+1}$  due to voltage differences  $V_{sus}$  between the even-numbered trigger electrodes  $T_2, T_4, T_6, \dots$  and the first sustaining electrodes  $S_2, S_4, S_6, \dots$ . Then, a voltage caused by charged particles produced at this time is added to a voltage difference between the trigger electrodes  $T_2, T_4, T_6, \dots$  and the second sustaining electrodes  $S_1, S_3, S_5, \dots$  to cause a secondary long-distance sustaining discharge. However, since a voltage difference between the odd-numbered trigger electrodes  $T_1, T_3, T_5, \dots$  and the sustaining electrodes  $S_1$  to  $S_{n+1}$  is not generated at the discharge cells of the odd-numbered trigger electrode  $T_n$ , a sustaining discharge is not generated.

Such a driving method is capable of preventing an erroneous discharge between the discharge cells provided with the adjacent sustaining electrode lines as well as obtaining an effect of high efficiency and high brightness according to a long-distance discharge, an increase of light-emission area and an increase of discharge frequency even though the barrier ribs are provided at the boundary portion between the discharge cells.

Fig. 12 and Fig. 13 are waveform diagrams for explaining another example of driving methods applied to the AC surface-

discharge PDP according to the third embodiment of the present invention.

In the PDP according to the third embodiment, when a pulse voltage applied to the sustaining electrodes  $S_n$  and  $S_{n+1}$  has a voltage level higher than a discharge initiating voltage  $V_{sus}$  required for the sustaining discharge, a selective sustaining operation may not be conducted normally. Driving waveforms for prevent this abnormal operation are shown in Fig. 12 and Fig. 13. In similarity to the driving method shown in Fig. 10 and Fig. 11, when the horizontal barrier ribs are provided between the sustaining electrode lines  $S_n$  and  $S_{n+1}$  of the PDP, the trigger electrode lines are divided into odd-numbered trigger electrode lines  $T_n$  and the even-numbered trigger electrode lines  $T_{n+1}$  for a driving.

Fig. 12 is waveform diagrams applied upon driving of the odd-numbered trigger electrode line  $T_n$  while Fig. 13 is waveform diagrams applied upon driving of the even-numbered trigger electrode line  $T_{n+1}$ .

As shown in Fig. 12 and Fig. 13, waveforms applied to the reset interval  $RP$  and the address interval  $AP$  are identical to those in Fig. 9 and Fig. 10. Upon driving of the odd-numbered trigger electrode line  $T_n$ , a scanning voltage pulse  $-V_s$  is applied to the even-numbered trigger electrode line  $T_{n+1}$  and, at the same time, a data pulse  $V_d$  is applied to each address electrode  $A_n$  in synchronization with the scanning voltage pulse  $-V_s$ , thereby causing an address discharge at the discharge cells  $C_n$  formed at the odd-numbered trigger electrode line  $T_n$  to select the discharge cells to be turned on. Upon driving of the even-numbered trigger electrode line  $T_{n+1}$ , a scanning voltage pulse  $-V_s$  is applied to the even-numbered trigger electrode line  $T_{n+1}$  and, at the same time, a data pulse  $V_d$  is applied to each address electrode  $A_n$  in synchronization with the scanning voltage pulse  $-V_s$ , thereby causing an address discharge at the discharge cells  $C_{n+1}$  formed at the even-numbered trigger electrode line  $T_{n+1}$ .

However, a waveform applied in the sustaining interval SP is different from that in Fig. 10 and Fig. 11.

First, with reference to the waveform diagrams of Fig. 12 applied to a driving of the odd-numbered discharge cell  $C_n$ , the same pulse waveform is applied to the odd-numbered trigger electrode line  $T_n$  and the even-numbered trigger electrode line  $T_{n+1}$  in the sustaining interval SP. However, the pulse waveforms applied to the odd-numbered and even-numbered trigger electrode lines  $T_n$  and  $T_{n+1}$  have a discharge initiating voltage  $V_{sus}$  having a high level. Herein, a low level is a desired voltage ( $V_b$ ) level between 0V and  $V_{sus}$  rather than a ground voltage level 0V. Furthermore, a voltage pulse  $V_a$  having a voltage level higher than the discharge initiating voltage  $V_{sus}$  is alternately applied to the odd-numbered sustaining electrode line  $S_n$  and the even-numbered sustaining electrode line  $S_{n+1}$ . When a high voltage level  $V_{sus}$  is applied to the trigger electrode lines  $T_n$  and  $T_{n+1}$  as shown in Fig. 12, the voltage pulse  $V_a$  is applied to the even-numbered sustaining electrode line  $S_{n+1}$ . On the other hand, when a low voltage level  $V_b$  is applied to the trigger electrode lines  $T_n$  and  $T_{n+1}$ , the voltage pulse  $V_a$  is applied to the odd-numbered sustaining electrode line  $S_n$ . According to such a pulse application method, a primary priming sustaining discharge is generated at the odd-numbered discharge cell  $C_n$  due to a voltage difference  $V_{sus}$  or  $V_a - V_b$  between the odd-numbered trigger electrodes  $T_1, T_3, T_5, \dots$  and the odd-numbered sustaining electrodes  $S_1, S_3, S_5, \dots$ . In this case, levels of  $V_a$  and  $V_b$  should be appropriately selected such that a value of  $V_a - V_b$  becomes more than the discharge initiating voltage. A priming effect of charged particles is added to a voltage difference ( $V_a - V_{sus}$  or  $V_b$ ) effect between the odd-numbered trigger electrode line  $T_n$  and the even-numbered sustaining electrode line  $S_{n+1}$  after the primary priming discharge was generated at the odd-numbered discharge cell  $C_n$ , thereby causing a secondary long-distance sustaining discharge. However, since a voltage difference ( $V_a - V_{sus}$  or  $V_b$ ) between the even-numbered trigger electrode line  $T_{n+1}$  and the

even-numbered sustaining electrode line  $S_{n+1}$  is lower than the discharge initiating voltage  $V_{sus}$  in a state in which charge particles are not produced, the first sustaining discharge is not generated at the even-numbered discharge cell  $C_{n+1}$ . As described above, the even-numbered discharge cell  $C_{n+1}$  does not generate a discharge upon driving of the odd-numbered discharge cell  $C_n$ , so that an erroneous discharge can be prevented even though the barrier ribs is not provided between the discharge cells and a selective sustaining discharge can be smoothly performed without any erroneous operation even though an excessive high voltage is applied to the sustaining electrodes.

Similarly, with reference to the waveform diagrams of Fig. 13 applied to a driving of the even-numbered discharge cell  $C_{n+1}$ , the same pulse waveform is applied to the odd-numbered trigger electrode line  $T_n$  and the even-numbered trigger electrode line  $T_{n+1}$  in the sustaining interval  $SP$ . Upon driving of the even-numbered discharge cell  $C_{n+1}$ , a high voltage level of the pulse waveforms applied to the odd-numbered and even-numbered trigger electrode lines  $T_n$  and  $T_{n+1}$  is a discharge initiating voltage  $V_{sus}$ , and a low voltage level thereof is a desired voltage ( $V_b$ ) level between  $0V$  and  $V_{sus}$  rather than a ground voltage level  $0V$ . When the high voltage level  $V_{sus}$  is applied to the trigger electrode lines  $T_n$  and  $T_{n+1}$  as shown in Fig. 13, a voltage pulse  $V_a$  is applied to the odd-numbered sustaining electrode line  $S_n$ . On the other hand, when a low voltage level  $V_b$  is applied to the trigger electrode lines  $T_n$  and  $T_{n+1}$ , the voltage pulse  $V_a$  is applied to the even-numbered sustaining electrode line  $S_{n+1}$ . According to such a pulse application method, a primary priming sustaining discharge is generated at the even-numbered discharge cell  $C_{n+1}$  due to a voltage difference  $V_{sus}$  or  $V_a - V_b$  between the even-numbered trigger electrodes  $T_{n+1}$  and the even-numbered sustaining electrodes  $S_{n+1}$ . A priming effect of charged particles is added to a voltage difference ( $V_a - V_{sus}$  or  $V_b$ ) effect between the even-numbered trigger electrode line  $T_{n+1}$  and the odd-numbered sustaining electrodes  $S_n$  after the

primary priming discharge was generated at the even-numbered discharge cell  $C_{n+1}$ , thereby causing a secondary long-distance sustaining discharge. However, since a voltage difference ( $V_a - V_{sus}$  or  $V_b$ ) between the odd-numbered trigger electrode line  $T_n$  and the odd-numbered sustaining electrode line  $S_n$  is lower than the discharge initiating voltage  $V_{sus}$  in a state in which charge particles have not been produced, the first sustaining discharge is not generated at the odd-numbered discharge cell  $C_n$ . As described above, the odd-numbered discharge cell  $C_n$  does not generate a discharge upon driving of the even-numbered discharge cell  $C_{n+1}$ , so that an erroneous discharge can be prevented even though the barrier ribs is not provided between the discharge cells and a selective sustaining discharge can be smoothly performed without any erroneous operation even though an excessive high voltage is applied to the sustaining electrodes.

Although the present invention has been explained by the embodiments shown in the drawings described above, it should be understood to the ordinary skilled person in the art that the invention is not limited to the embodiments, but rather that various changes or modifications thereof are possible without departing from the spirit of the invention. Accordingly, the scope of the invention shall be determined only by the appended claims and their equivalents.